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中国深层—超深层页岩气压裂:问题、挑战与发展方向

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摘要:中国历经 10 余年的页岩气压裂理论创新与工程实践,已形成中浅层($<3500\text{ m}$)海相页岩气压裂理论与技术体系,支撑了海相页岩气规模效益开发。中国深层($3500\sim4500\text{ m}$)—超深层($>4500\text{ m}$)页岩气技术可采资源量占页岩气总可采资源量的 56.63%,实现高效开发是页岩气产业发展和保障油气安全的主战场;四川盆地及其周缘深层—超深层页岩气可采资源量占其总可采资源量的 65.8%,是高效开发页岩气和建设“气大庆”的主阵地。基于中国深层—超深层页岩气压裂的前期探索与实践认识,根据深层—超深层页岩气压裂的 10 大特征,分析了由此衍生并亟待解决的 6 个基础问题或面临的挑战,提出了亟需创新的 5 个关键理论和方法,指出了深层—超深层页岩气压裂的 10 个发展方向,并强调:中国页岩气开发要“深浅并重”,中浅层要继续规模建产和提高采收率;深层—超深层要实现高效开发,进军深层—超深层机遇和挑战并存,尚需不断“砺剑”,加快建立中国深层—超深层页岩气压裂理论与技术体系。

关键词:深层—超深层;页岩气;压裂;问题和挑战;发展方向

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Deep and ultra-deep shale gas fracturing in China: problems, challenges and directions

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Abstract: After more than 10 years of theoretical innovation and engineering practice in shale gas fracturing, supporting the scale cost-effective development of marine shale gas, China has established a theoretical and technical system for marine shale gas fracturing in the middle and shallow layers ($<3500\text{ m}$). The technically recoverable resources of deep ($3500\sim4500\text{ m}$) and ultra deep ($>4500\text{ m}$) shale gas in China account for 56.63% of the total recoverable shale gas reserve. To achieve efficient gas exploitation is essential for the development of the shale gas industry and guarantee of oil and gas security. The recoverable resources of deep ($3500\sim4500\text{ m}$) and ultra deep ($>4500\text{ m}$) shale gas in Sichuan Basin and its periphery account for 65.8% of the total reserve, making the most important contribution to the efficient development of shale gas and the construction of “Daqing Gas Base”. Based on the preliminary exploration and practical understanding of deep and ultra deep shale gas fracturing in China and according to the 10 characteristics of deep and ultra deep shale gas fracturing, this paper analyzes six basic problems or challenges that are derived from above situation and urgently need to be solved. Further, the paper proposes five key theories and methods that urgently need to be innovated, points out 10 development directions for deep and ultra deep shale gas fracturing, and emphasizes that China’s shale gas development should focus on both deep and shallow layers and continue to improve large-scale production and EOR in the middle and shallow layers. There are both opportunities and challenges in advancing into the new fields of exploration in deep and ultra deep layers to achieve ef-

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ficient development. It is still necessary to continuously enhance the research, and accelerate the establishment of China's fracturing theory and technology system for deep and ultra deep shale gas.

Key words: deep and ultra deep layer; shale gas; fracture; problem and challenge; development direction

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美国从1965年实施第一口页岩气直井小规模压裂、1991年实施第一口页岩气水平井多段压裂、1997年实施第一口页岩气直井滑溜水压裂、1999年首次提出缝网(network fractures)概念、2002年实施第一口页岩气水平井滑溜水多段压裂、2006年首次提出体积压裂(stimulated reservoir volume, SRV)概念、2009年首次提出减小簇间距, 到2012年全面推广水平井多段多簇压裂, 再到近10余年不断发展新工具、新材料、新工艺, 历经半个多世纪, 压裂技术的进步推动了美国页岩气革命取得巨大成功^[1-2], 改变了世界能源格局。2022年, 美国页岩气产量达到 $7950 \times 10^8 \text{ m}^3$, 占全球页岩气总产量的94.6%。

2012年, 美国Breakthrough Institute指出, 美国通过数十年研究, 攻克了页岩气压裂难题, 中国页岩气压裂才刚刚起步^[3]。2010年中国首次实施海相页岩气直井(方深1井、威201井)压裂^[4-5], 2011年首次实施海相页岩气水平井(威201-H1井、建页HF-1井)压裂^[6-7]。初期的页岩气压裂基本上都是外国公司提供技术服务, 中国公司承担现场施工。陕西延长石油(集团)有限责任公司从2011年开始在鄂尔多斯盆地开展陆相页岩气直井和水平井(柳坪177井、延页平1井)压裂试验^[8]。尽管是以跟踪学习、吸收消化美国技术为主, 但中国石油天然气集团有限公司(中国石油)在初期创造了一系列页岩气压裂的全国第一, 后因常规天然气勘探开发任务重, 放缓了页岩气压裂节奏;伴随着涪陵地区的焦页1HF井(涪陵页岩气功勋井)压裂获高产工业气流, 中国石油化工集团有限公司(中国石化)也加快了页岩气压裂步伐。

2008年, 唐嘉贵等^[9]发表的探讨页岩气勘探开发技术的论文提出了页岩气压裂沟通天然裂缝的思路;2008年, 任岚^[10]开展了缝网压裂机理研究, 并完成有关非常规油气藏缝网压裂的博士论文;2009年, 赵金洲等与大庆油田合作进行了缝网压裂项目——《海拉尔火山岩布达特组缝网压裂机理研究》, 开展了缝网压裂现场试验;2009年, 雷群等^[11]提出了低渗特低渗油气藏缝网压裂技术;2011年, 吴奇等^[12]在调研美国页

岩气压裂技术现状的基础上, 提出了中国页岩气压裂技术未来发展方向;2012年, 赵金洲等^[13]从压裂改造的角度分析了页岩气储层基本特征, 阐述了页岩气藏压裂理论、材料和工艺面临的难题和挑战, 提出了页岩气藏改造技术关键, 并掀起了页岩气压裂研究和实践的高潮。历经10余年, 中国已创建了中浅层($<3500 \text{ m}$)页岩气水平井压裂理论与技术体系, 实现了中国页岩气压裂技术从无到有、从跟跑到并跑的重大跨越, 推动了中国页岩气勘探开发取得重大突破^[14-17], 建成重庆涪陵、四川长宁—威远、滇黔北昭通3个国家级海相页岩气示范区和延长石油延安国家级陆相页岩气示范区, 页岩气产量从2012年的 $0.25 \times 10^8 \text{ m}^3$ 增长到2022年的 $240 \times 10^8 \text{ m}^3$, 成为仅次于美国的全球第二大页岩气生产国^[18-20]。

中国页岩气技术可采资源为 $19.36 \times 10^{12} \text{ m}^3$, 深层($3500 \sim 4500 \text{ m}$)—超深层($>4500 \text{ m}$)占56.63%^[21]。中浅层页岩气能否继续稳产上产和提高采收率, 是中国页岩气发展的“压舱石”;深层—超深层页岩气能否有效开发, 是中国页岩气发展的主战场。中浅层海相页岩气已基本完成产能建设, 要持续规模建产;深层—超深层页岩气已显示出巨大的开发潜力, 要持续加强攻关, 向深层—超深层进军, 但机遇和挑战并存, 尚需不断“砺剑”。与中浅层相比, 深层—超深层特别是四川盆地及其周缘深层—超深层页岩储层多位于复杂构造区^[22], 褶皱和断裂增加, 地应力复杂及水平应力差大^[23], 埋藏深、温度高、压力高、基质致密、非均质性强、岩石微观孔隙结构复杂和含气差异性大, 勘探开发面临极大挑战^[24], 储层有效压裂改造是深层—超深层页岩气高效开发的关键, 需要不断探索适应深层—超深层页岩气的压裂理论及技术对策^[25-28]。

笔者基于中国深层—超深层页岩气压裂的前期探索与实践认识, 解析高效压裂面临的问题和挑战, 提出了高效压裂急需构建的关键理论和方法, 指出了深层—超深层页岩气压裂发展方向, 以期为建立中国深层—超深层页岩气压裂理论与技术体系提供参考。

1 深层—超深层页岩气勘探及压裂实践

四川盆地及其周缘深层—超深层页岩气资源量占其总资源量的70%以上,技术可采资源量占总可采资源量的65.8%^[29],是页岩气勘探开发的主力军,也是决定能否建成“气大庆”的关键。

中国石化在发现涪陵页岩气田以后即针对深层页岩气开展前瞻性研究和勘探实践,优选丁山地区部署实施了丁页2HF井(埋深为4417 m),2013年12月压裂测试获产气量为 $10.5 \times 10^4 \text{ m}^3/\text{d}$,这是中国首口获得深层工业气流的页岩气井,也是中国首次在埋深大于4 000 m的储层发现页岩气^[30];2019年1月,重庆綦江东溪构造东页深1井(埋深为4 270 m)压裂测试获产气量为 $31.2 \times 10^4 \text{ m}^3/\text{d}$,这是中国埋深大于4 200 m的首口高产页岩气井;2022年6月,在位于重庆万盛地区的新页1井(埋深为3 757 m)压裂测试获产气量为 $53.2 \times 10^4 \text{ m}^3/\text{d}$,至此形成中国石化川东南盆缘复杂构造带“新场南—东溪—丁山—林滩场”整体连片^[31],页岩层段的资源总量达到 $1.19 \times 10^{12} \text{ m}^3$,2022年綦江深层页岩气田提交首批探明地质储量为 $1459.7 \times 10^8 \text{ m}^3$ 。2015年8月,在位于四川威远地区的威页1HF井(埋深3 622 m)压裂测试获产气量为 $17.5 \times 10^4 \text{ m}^3$,成为中国石化深层页岩气勘探开发的标志性突破;2017年10月,威页23-1HF井(埋深为3 838 m)压裂测试获产气量为 $26 \times 10^4 \text{ m}^3/\text{d}$;2018年,发现中国首个主体埋深超过3 700 m的深层页岩气田——威荣页岩气田,提交探明储量为 $1247 \times 10^8 \text{ m}^3$,同步启动产能建设^[24,32-33]。

2017年8月,中国石油在位于重庆大足的足201-H1井(埋深为4 372 m)压裂获产气量为 $10.6 \times 10^4 \text{ m}^3/\text{d}$,发现渝西深层页岩气区块^[34]。2018年8月,在位于四川江安县的泸202井(埋深为4 324 m)压裂获产气量为 $13.2 \times 10^4 \text{ m}^3/\text{d}$,发现泸州深层页岩气区块;2019年3月,在位于四川泸县的泸203井(埋深为3 892 m)压裂测试获产气量为 $137.9 \times 10^4 \text{ m}^3/\text{d}$,刷新了中国页岩气井最高日产量纪录,也是中国首口单井测试日产量超百万立方米的页岩气井;2020年1月,在位于四川泸县的阳101H4-5井(埋深为4 058 m)压裂测试获产气量为 $32.1 \times 10^8 \text{ m}^3/\text{d}$;2021年,泸州区块新增探明地质储量为 $5138.1 \times 10^8 \text{ m}^3$,落实了中国首个万亿立方米储量的深层页岩气区^[17,35]。

近两年,中国石化和中国石油又先后在页岩气新区取得页岩气勘探重大突破^[17,36-37]。2022年9月,中国石化在四川乐山井研—犍为地区的金石103HF井(埋深为3 920 m)压裂测试获产气量为 $25.86 \times$

$10^4 \text{ m}^3/\text{d}$,首次在四川盆地寒武系筇竹寺组取得重大勘探突破,评价落实页岩气地质资源量为 $3878 \times 10^8 \text{ m}^3$,整个页岩层段资源量超过 $1 \times 10^{12} \text{ m}^3$ 。2023年2月,中国石油在四川资阳地区的资201井(埋深为4 603 m)压裂测试获产气量为 $73.88 \times 10^4 \text{ m}^3/\text{d}$,实现了寒武系筇竹寺组页岩气的高产突破,建产有利区面积超3 000 km²,页岩气资源量近 $2 \times 10^{12} \text{ m}^3$ 。2020年10月,中国石化在湖北利川盆地红星地区的红页1HF井吴家坪组压裂测试获产气量为 $8.93 \times 10^4 \text{ m}^3/\text{d}$,填补了中国二叠系页岩气勘探开发的空白;2021年9月,在红页2HF井(埋深为4 000 m)压裂试气,试采产量保持稳定,提交红星地区二叠系首批页岩气预测储量为 $1051 \times 10^8 \text{ m}^3$ 。2022年10月,中国石油在川东地区梁平的大页1H井(埋深为4 339 m)二叠系吴家坪组压裂获产气量为 $32.06 \times 10^4 \text{ m}^3/\text{d}$,有利勘探区面积为2 885 km²,页岩气资源量达 $1 \times 10^{12} \text{ m}^3$ 。

随着深层页岩气勘探的不断发现,深层页岩气压裂研究快速跟进,压裂建产初见成效,但压裂效果差异明显(表1),压后效果主控因素不明、缝网扩展机理不清、缝网设计方法不适应、压裂工艺缺乏针对性。

2 深层—超深层页岩气压裂问题或挑战

以川南地区五峰组—龙马溪组一段为例,与中浅层页岩储层相比,深层—超深层储层的构造特征以低陡构造和低幅褶皱构造为主,断层发育,压裂的地质工程条件更为复杂^[38-39],表现为地层温度高、地层压力高、破裂压力高、延伸压力高、闭合压力高、施工压力高、地应力差大、裂缝欠发育、岩石脆性弱、岩石塑性强等10大特征(表2),使得裂缝更难压开、裂缝更难延伸、裂缝更难转向、裂缝更难支撑,从而导致缝网建造难度更大,缝网支撑有效性更低,并且受断层、高应力环境、天然地震等影响,部分井段出现套变及压窜等问题。

根据10大特征,深层—超深层页岩气压裂可以归纳为面临6个挑战或必须解决6个基础问题,具体目标就是形成“人造气藏”,建造高复杂度有效缝网,形成“国道—省道—县道—乡道—村道”路路通的页岩气流动“高速公路网”。

2.1 高围压页岩破裂向单一裂缝演进,缝网形成困难

岩石力学三轴实验表明^[40-41],围压(σ_c)为0~15 MPa时,以多裂纹劈裂为主;围压为30~45 MPa时,以多条张性和剪性裂纹为主;围压在60 MPa以上时,以单裂纹为主(图1),深层—超深层页岩压裂形成分支缝难度大。

表 1 四川盆地典型深层页岩区块部分井压裂效果

Table 1 Fracturing effects of some wells in typical deep shale blocks in Sichuan Basin

气田、区块	井号	埋深/m	压裂时间	测试产量/ (10 ⁴ m ³ /d)	气田、区块	井号	埋深/m	压裂时间	测试产量/ (10 ⁴ m ³ /d)
中国石化 威荣气田	威页 1HF	3 622	2015-08	17.5	中国石化 丁山—东溪区块	丁页 2HF	4 417	2013-12	10.5
	威页 23-1HF	3 838	2017-10	26.0		丁页 5	4 146	2017-12	16.3
	威页 43-4HF	3 796	2019-08	74.3		东页深 1	4 270	2019-01	31.2
	威页 43-3HF	3 779	2019-08	11.4		东页深 3	4 400	2020-09	0.14
	威页 39-7HF	3 831	2020-05	10.0		丁页 5-1HF	3 752	2021-11	19.4
	威页 34-3HF	3 768	2021-08	23.4		东页深 4	4 186	2021-04	2.0
	威页 41-6HF	3 798	2021-01	4.8		东页深 2	4 242	2021-10	41.2
	威页 24-3HF	3 784	2021-11	6.8		丁页 7	4 462	2021-12	42.8
	威页 25-2HF	3 824	2022-06	13.5		丁页 9	3 800	2022-01	12.0
	威页 31-9HF	3 747	2022-04	7.9		丁页 2-1HF	4 428	2023-01	55.2
中国石油 泸州区块	泸 201	3 675	2018-07	1.8	中国石油 渝西区块	足 202	3 657	2017-07	4.9
	泸 202	4 324	2018-08	13.2		足 201-H1	4 372	2017-08	10.6
	泸 203	3 892	2018-12	137.9		足 202-H1	3 925	2018-05	45.7
	泸 204	3 819	2019-02	14.4		黄 202	4 018	2018-03	22.4
	阳 101H2-8	4 107	2019-11	50.7		足 202H2-2	4 018	2019-11	6.2
	泸 206	4 049	2020-01	30.6		足 203H1-1	4 138	2020-05	20.2
	泸 205	4 070	2020-04	20.3		足 203H1-3	4 213	2020-05	23.7
	阳 101H1-8	3 722	2020-10	20.1		黄 202H3-2	4 268	2020-09	8.7
	阳 101H26-3	4 004	2020-10	28.3		足 207	4 381	2020-12	14.2
	泸 209	3 739	2021-02	13.2		黄 202H1-4	4 089	2020-12	6.0

表 2 四川盆地南部页岩气储层地质工程参数对比

Table 2 Comparison of geoengineering parameters of shale gas reservoirs in the Southern Sichuan Basin

储层	地层温度/ ℃	地层压力/ 系数	破裂压力/ MPa	延伸压力/ MPa	闭合应力/ MPa	施工压力/ MPa	水平应力差/ MPa	天然微裂缝	脆性指数	杨氏模量/ GPa	泊松比
中浅层	90~120	1.2~2.0	80~100	50~90	45~70	68~93	9~18	较发育	>0.60	35~48	0.19~0.24
深层—超深层	120~150	1.8~2.2	120~130	95~120	90~100	95~120	15~25	欠发育	<0.44	19~23	0.21~0.25
深层—超深层特征	地层温度高	地层压力高	破裂压力高	延伸压力高	闭合压力高	施工压力高	地应力差大	裂缝欠发育	岩石脆性弱、岩石塑性强		

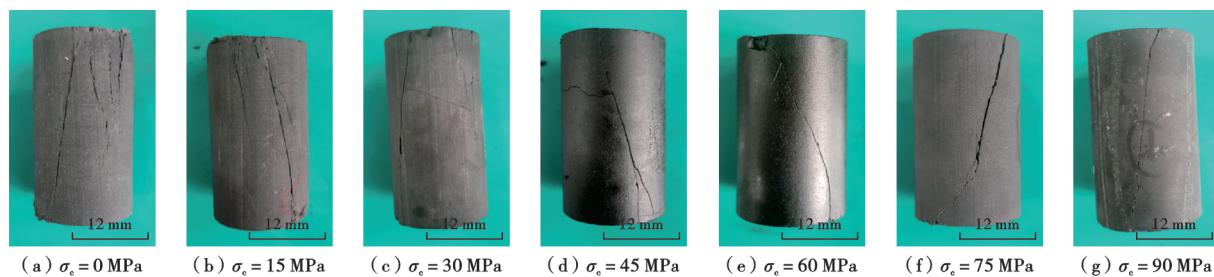


图 1 不同围压下页岩破裂特征

Fig. 1 Fracture features of shale under various confining pressures

低围压下岩样在峰值点破裂后应力迅速跌落,弹性势能迅速释放,呈脆性特征;高围压下岩样在峰值点破坏后应力跌落较慢,仍有部分弹性势能储存内部,随围压增加逐渐表现出塑性特征(图 2)^[41-42],缝网形成难度大。深层—超深层页岩破裂还受岩性、温度和内部结构等多重因素影响,破裂模式及弹脆性演进更趋复杂。

2.2 页岩黏弹塑性变形行为复杂,破裂规律不明

岩石力学三轴实验、页岩蠕变实验^[43]表明,深层—超深层页岩在高温高压环境下黏弹性变形行为与

弹塑性破裂机理复杂,页岩力学性能受到温度、湿度和应力等环境影响,会发生蠕变、刚度退化、塑性屈服、时间依赖和路径相关等力学行为(图 3)。

页岩水化实验表明^[44-45],页岩水化后抗拉强度降低,矿物颗粒间黏聚力减弱,矿物溶蚀、脱落,扩大溶蚀孔缝和产生新的微细裂缝(图 4),增加应力弱点或弱面,有可能增加裂缝起裂点和扩展路径,从而提升缝网复杂程度。深层—超深层页岩黏弹塑性变形行为认识不清,不同力学加载下的破裂规律不明。

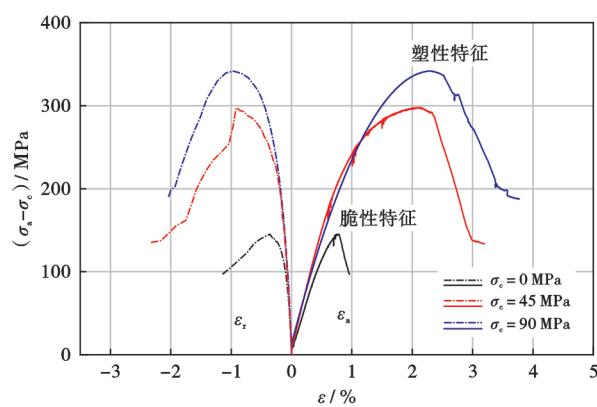
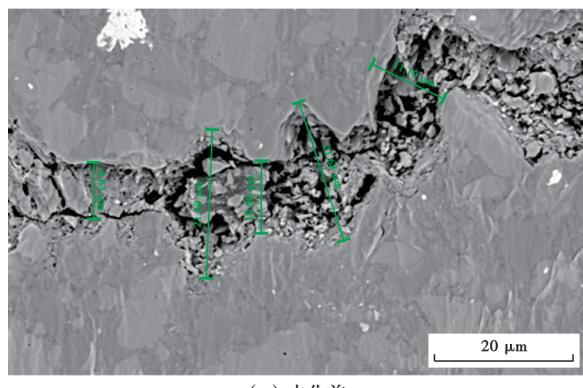


图 2 不同围压下页岩压缩应力—应变曲线

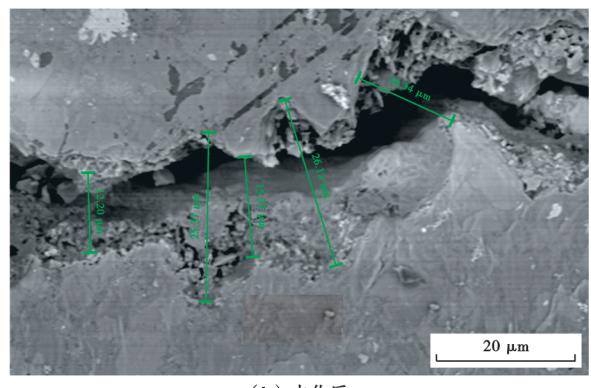
Fig. 2 Compressive stress-strain curves of shale under different confining pressures

2.3 裂缝动态扩展机理不清,延伸规律不明

深层—超深层页岩在黏性、弹性、塑性交互作用下,裂缝尖端钝化、扩展阻力增大,高温高压效应抑制天然裂缝(裂隙)开启扩展,难以发育复杂缝网。在高温和高应力环境下,深层—超深层页岩的非线性破裂



(a) 水化前



(b) 水化后

图 4 页岩水化前后孔隙结构

Fig. 4 Pore and fracture structure before and after shale hydration

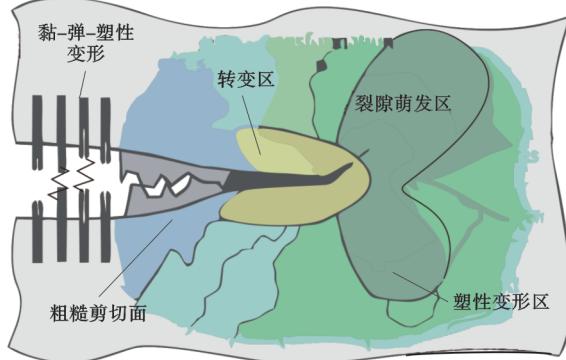


图 5 黏弹性作用下裂缝尖端扩展(据文献[46]修改)

Fig. 5 Crack tip propagation under visco-elasticity plasticity

2.4 复杂构造下缝网建造困难,控制机制不明

深层—超深层页岩褶皱、断层发育,复杂构造改变

机制及本构关系尚未构建,非线性破裂机制下的裂缝动态扩展机理不清^[46](图 5),裂缝扩展模型有待发展,裂缝扩展影响因素无法定量表征,耦合工程条件下的裂缝扩展规律不明。

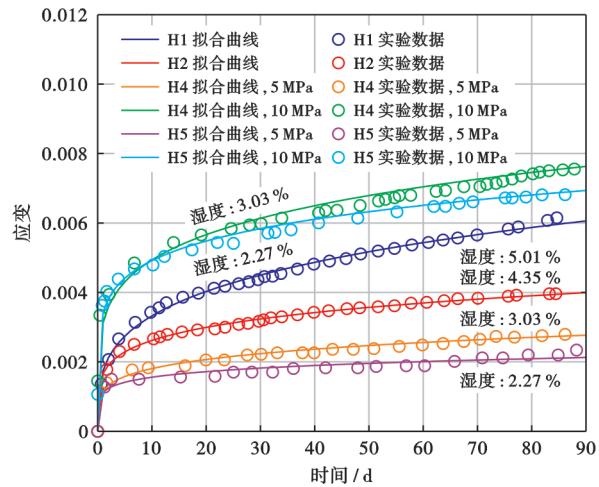
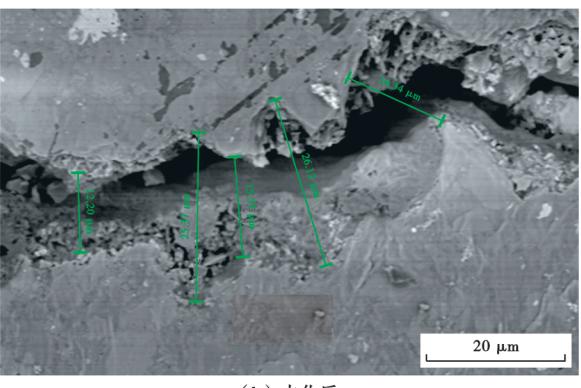


图 3 应力和湿度对岩石蠕变行为的影响(岩心 H1-5)

Fig. 3 Effect of stress and humidity on creep behaviors of rocks



(b) 水化后

图 4 页岩水化前后孔隙结构

局部应力分布和天然裂缝群分布,不同类型构造对局部应力的影响也存在本质差异^[47-48],叠加深层—超深层页岩原始应力,加剧储层应力分布的非均匀性,结合井筒与构造的空间关系,不同构造、不同井筒布置下的缝网建造差异大,控制机制有待揭示(图 6)^[49-51]。

2.5 缝网导流存在多重力学作用,渐变规律不清

高温高压环境下页岩流变特征行为显著,裂缝壁面与支撑剂之间存在长期蠕变、破坏,支撑剂颗粒挤压、压实、嵌入、破碎等非线性非连续多重力学作用行为(图 7)^[52-53]。支撑剂颗粒与页岩非线性力学作用下的水力裂缝支撑宽度不足,支撑剂运移铺置困难,支撑剂颗粒在深层页岩复杂缝网中的空间展布不均匀,有效支撑受到抑制。闭合应力高,支撑剂嵌入和破碎对缝网长期导流影响严重^[54],导流渐变规律不清。

2.6 钻井压裂套管变形形成因多样,套变机制不清

川南地区深层页岩气受区域断层、天然地震和高应力环境影响,套变工程风险与管控是面临的新问题。由于天然裂缝带在部分区域集中发育,空间展布复杂,导致套管变形和压窜频发(图8),如泸203井区(截至

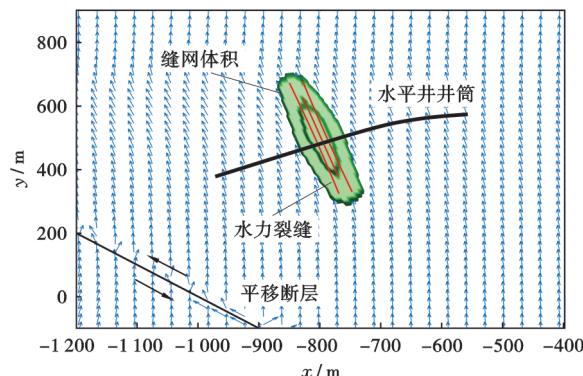


图 6 断层局部应力影响的缝网扩展模拟

Fig. 6 Simulation of fracture network expansion under the influence of local stress on faults

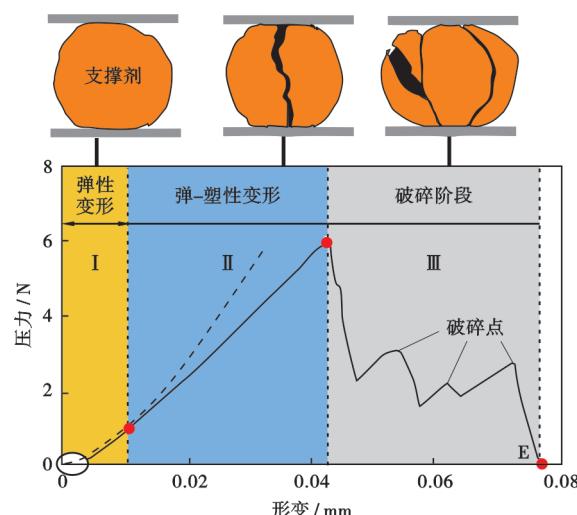


图 7 支撑剂受压加载条件下的压力—形变关系^[53]

Fig. 7 Pressure-deformation relationship of proppant under compression loading conditions

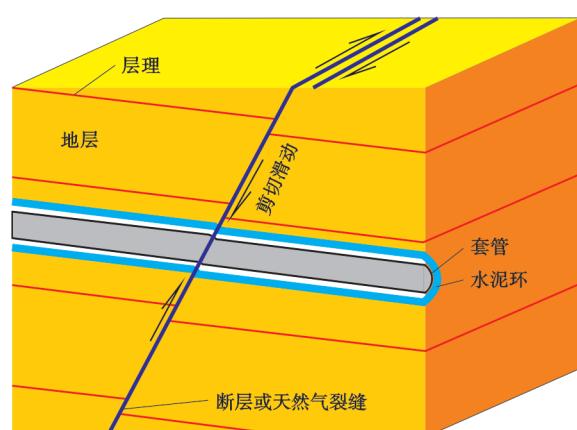


图 8 断层剪切滑动诱发套管变形

Fig. 8 Casing deformation induced by shearing slip of faults

2022年5月)完钻井96口,套变60口(含27口未压先变井)。套变导致压裂分段工具难以下入,由于压裂套变机理不清^[55-58],防控措施和工程方法欠缺,严重影响水平井段压裂改造的完整性和充分性。

3 深层—超深层页岩气压裂关键理论和方法

深层—超深层页岩气高效压裂亟待构建缝网综合可压性评价、缝网动态演化扩展、支撑剂远距离输送及长效支撑、套变工程控制、实时监测裂缝与压后评价等关键基础理论和方法。

3.1 缝网综合可压性评价理论和方法

缝网综合可压性由岩石脆性可压性、天然弱面发育、缝网扩展能力和含气性4个因子构成^[59],其中,脆性可压性基本采用矿物^[60-62]或力学参数^[63-65]脆性评价方法计算,但深层—超深层高温高围压下页岩力学性质发生显著改变^[66-67],页岩由脆性变形向亚脆性变形过渡^[68],需要发展基于岩石动态破坏过程描述的脆性评价方法^[41,69-71],才能有效表征岩石破坏过程中的全应力—应变响应^[72-73]。缝网扩展能力需结合页岩黏弹塑性变形行为破坏表征进行完善^[74],构建深层—超深层缝网综合可压性评价理论和方法。

3.2 复杂构造下的缝网动态演化扩展理论

深层—超深层页岩具有非线性破裂特征,裂缝扩展准则需要修正。复杂构造影响应力和天然裂缝非均匀分布,压裂簇裂缝异步起裂^[75-76],裂缝在非均匀应力环境下可能从低应力向高应力、或从高应力向低应力扩展^[77-79];高应力差下裂缝簇间距小,簇裂缝存在强应力干扰^[80-81]。准确模拟表征深层—超深层页岩气压裂缝网扩展规律需要发展复杂构造下缝网动态演化扩展理论^[82-84]。

3.3 高闭合应力下缝网支撑剂输运理论和铺置方法

高闭合应力作用下^[85-86],裂缝自支撑导流能力极低,相比中浅层相同铺砂浓度下支撑裂缝导流能力更弱^[87-89]。更大的支撑裂缝面积和更高的铺砂浓度是取得压裂效果的基础,但深层—超深层压裂裂缝宽度小,高浓度支撑剂进入困难,特别是分支缝和张开的天然裂缝更难得到支撑,缝网有效支撑和支撑剂进入困难矛盾凸显。压后生产作用在裂缝的有效闭合应力增加,加剧支撑剂压实、形变、嵌入以及岩石蠕变^[90-91],导流能力保持更加困难^[92]。需要准确描述支撑剂在高闭合应力下的力学行为特征,研发新型支撑材料,开展裂缝壁面—支撑剂颗粒多重力学行为仿真研究,建立缝网支撑剂输运理论和铺置方法,实现缝网长期有效支撑^[93-97]。

3.4 压裂套变机制和工程控制方法

诱发套变主要由套管强度降低和外部载荷变化两个因素引起^[98-99],页岩气压裂套变与天然断层激活滑移直接相关^[100-104],地应力场、断层产状、孔隙压力是影响断层稳定性的主要因素^[105-109]。需要结合储层地质力学环境表征、断层位移发生临界条件、井筒变形强度等理论揭示压裂套变机制,构建压裂套变工程控制方法,为优化压裂套变风险井施工参数设计提供基础。

3.5 实时裂缝监测方法与压后评价理论

簇裂缝延伸动态实时监测是裂缝调控的基础,实现边监测边调控。目前页岩气压裂监测以改造体积和支撑剂空间分布评价为主^[110-114],主要用于压后评价,压后评价也发展了施工曲线诊断识别方法^[115],但无法对分簇裂缝延伸进行实时监测和动态评价调控。最新发展的井筒听诊器^[116-118]和分布式光纤监测技术^[119-121]初步实现了实时连续监测,但亟需建立

联合实时监测解释的裂缝均衡延伸调控及压后评价理论。

4 深层—超深层页岩气压裂发展方向

建立完善深层—超深层页岩气压裂理论和技术体系有许多工作要做,在技术层面要开展10个方面的研究,这也是深层—超深层页岩气压裂技术的重点发展方向。

4.1 应力场和天然裂缝分布研究

深层—超深层环境下复杂构造导致的复杂应力场以及钻井、压裂诱导应力场变化是井眼轨迹优化、复杂缝网设计、套变压窜防控的基础。深层—超深层页岩复杂构造应力场影响机制与局部非均匀应力场表征研究尚不充分,受钻井井眼应力干扰与压裂簇裂缝延伸诱导应力叠加影响,深层页岩储层应力场的准确表征更为复杂(图9)^[122],需要开展复杂构造影响下的应力场变化机制以及钻井、压裂诱导应力场分布规律研究。

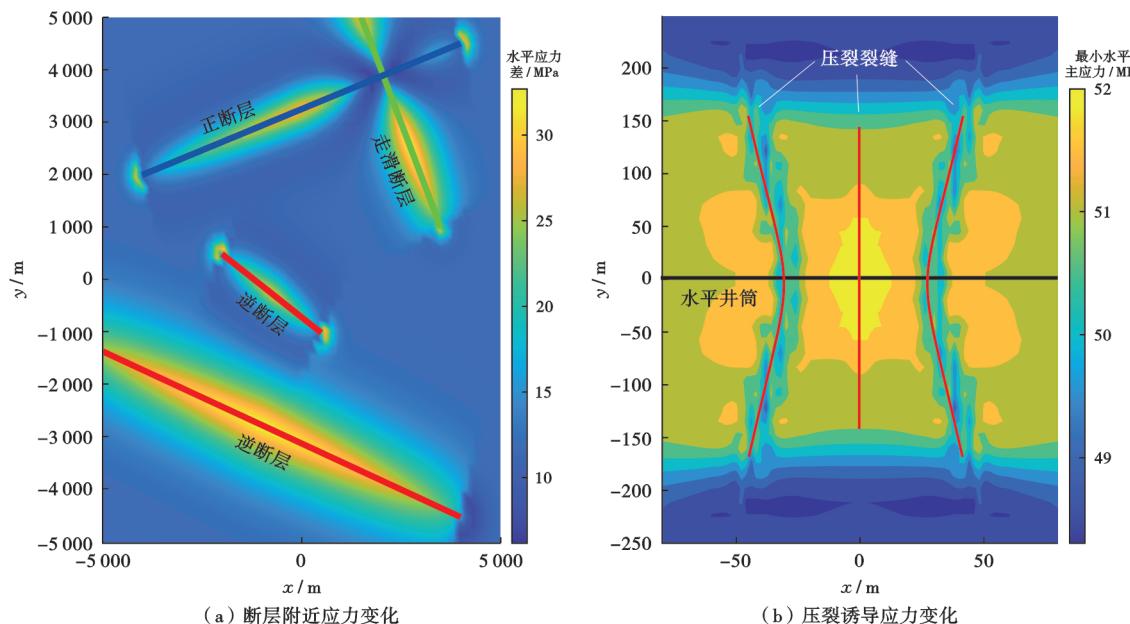


图9 断层附近和压裂诱导应力变化

Fig. 9 Stress changes near faults and induced by fracturing

天然裂缝是能否压成复杂缝网系统(压裂主裂缝+分支缝+张开的天然裂缝)的关键要素(图10)^[123],天然裂缝系统分布规律、天然裂缝产状及力学参数定量表征是压裂方案科学设计的核心基础,因此需要开展天然裂缝分布研究。

4.2 压裂缝网建造理论与优化设计方法

缝网建造是深层—超深层页岩气压裂的关键。需要建立温度—应力—湿度场多场耦合作用的黏—弹—塑性本构方程,开展真三轴多簇压裂物理模拟,开展页岩黏弹性变形行为与弹塑性多尺度破裂模式、缝网演化机制与控制机理、缝网压裂数值模拟研究(图11)^[124],

建立深层—超深层页岩气压裂缝网建造理论。

基于地质—工程一体化,开展缝网质量主控因素评价、缝网压裂参数优化设计方法、缝网支撑剂输运铺置和缝网建造工艺技术研究^[125-126]。

4.3 促进裂缝均衡延伸调控技术

深层—超深层页岩气压裂时,高地应力差导致裂缝簇间距更小,簇裂缝应力干扰效应增强,同时受井筒应力和力学参数非均质性分布影响,簇裂缝非均匀延伸极其严重,部分裂缝延伸过长,部分裂缝延伸不足甚至无法起裂,严重影响缝网建造质量。需要发展缝口暂堵转向裂缝延伸理论模型,优化暂堵时机、暂堵材料

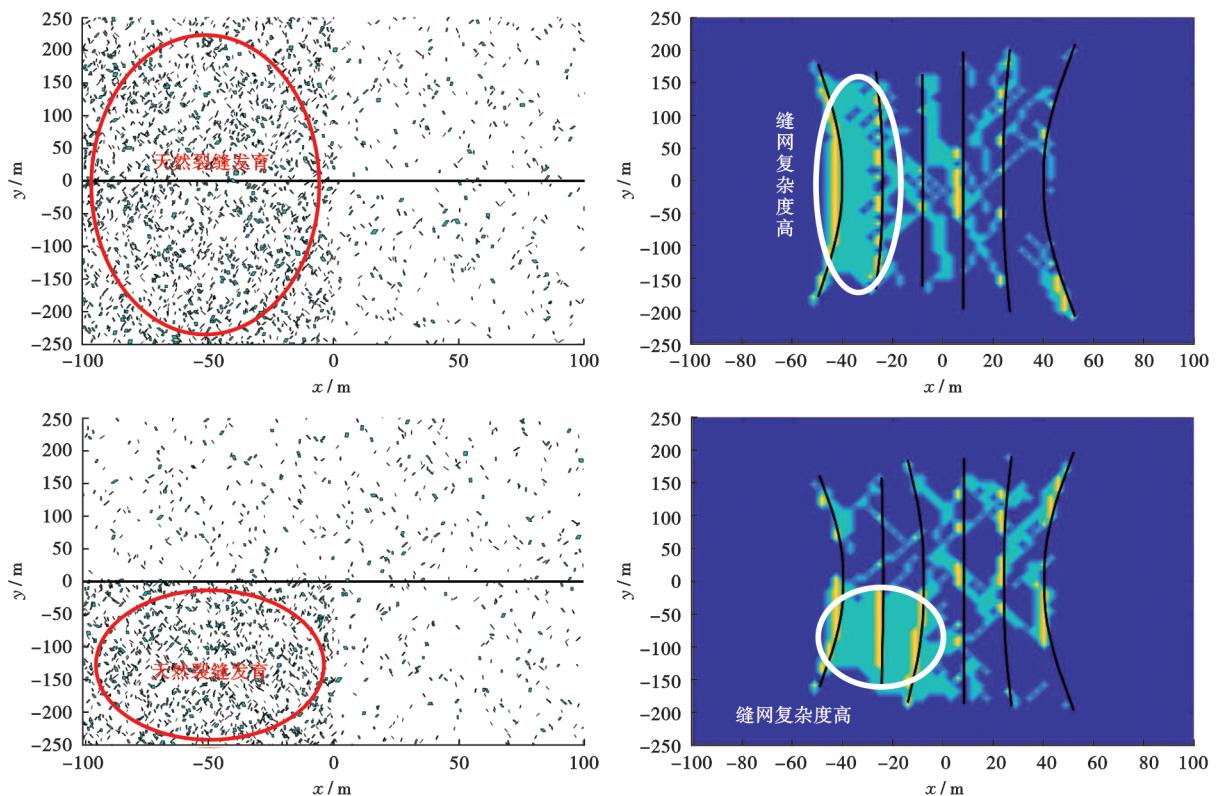
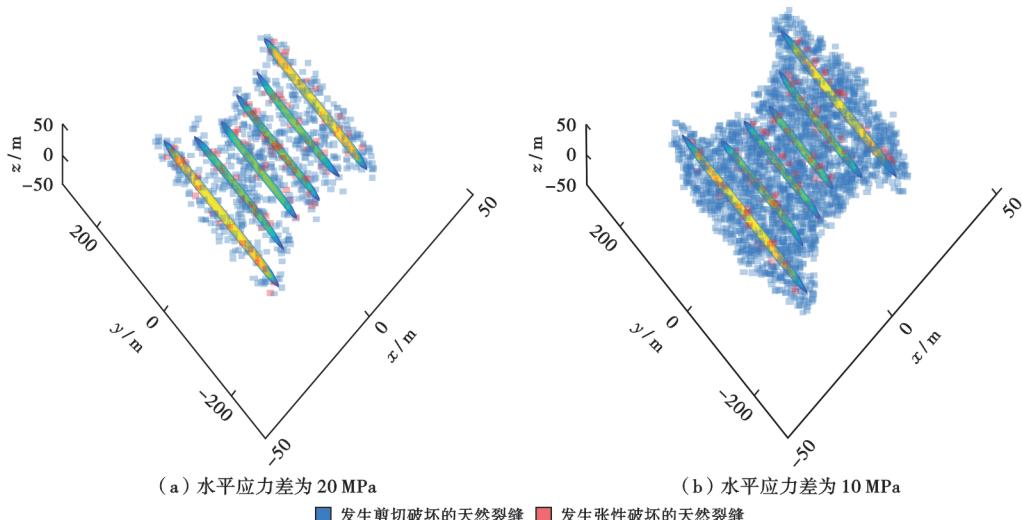


图 10 天然裂缝发育与复杂缝网展布模拟

Fig. 10 Simulation of natural fracture development and complex fracture network distribution



注:条带表示水力裂缝,颜色越接近黄色,缝宽越大;颜色越接近蓝色,缝宽越小。

图 11 水平应力差对缝网扩展的影响

Fig. 11 Effect of horizontal stress difference on the expansion of fracture network

用量、暂堵次数等核心参数设计方法,建立促进裂缝均匀延伸调控技术(图 12)^[127-128],实现多簇裂缝“抑长促短、均匀延伸”。

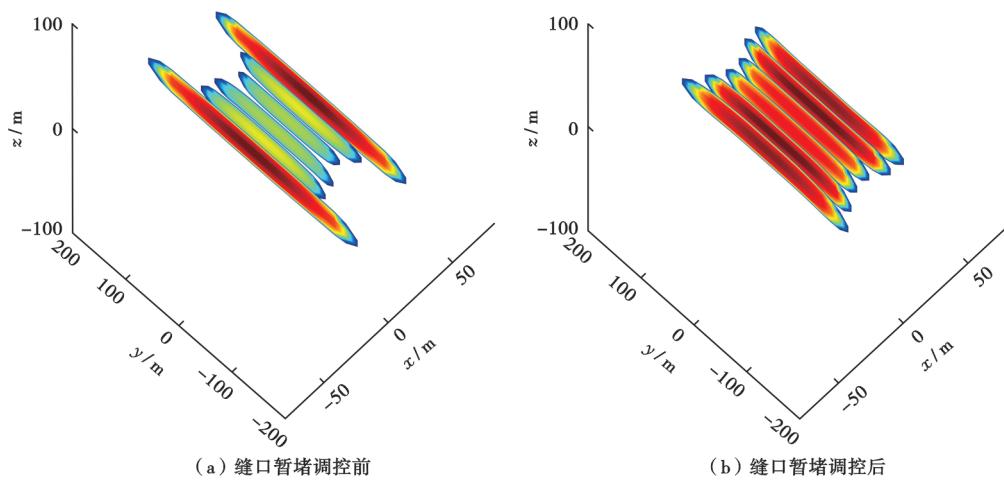
4.4 提高缝网复杂度调控技术

深层—超深层页岩破裂向单一裂缝演进,弹脆性趋弱,分支缝扩展阻力增大,天然裂缝开启扩展困难,同时水平应力差较大,主裂缝内净压力不能大规模激活天然裂缝和层理缝,缝网复杂程度降低。需要发展

缝内暂堵转向缝网扩展理论模型,优化暂堵材料用量和暂堵时机设计方法,建立提高缝网复杂度的调控技术(图 13)^[127,129],提升缝内净压力,扩大分支裂缝与天然裂缝激活规模,提高缝网复杂度。

4.5 研发深层—超深层页岩气新型压裂液体系

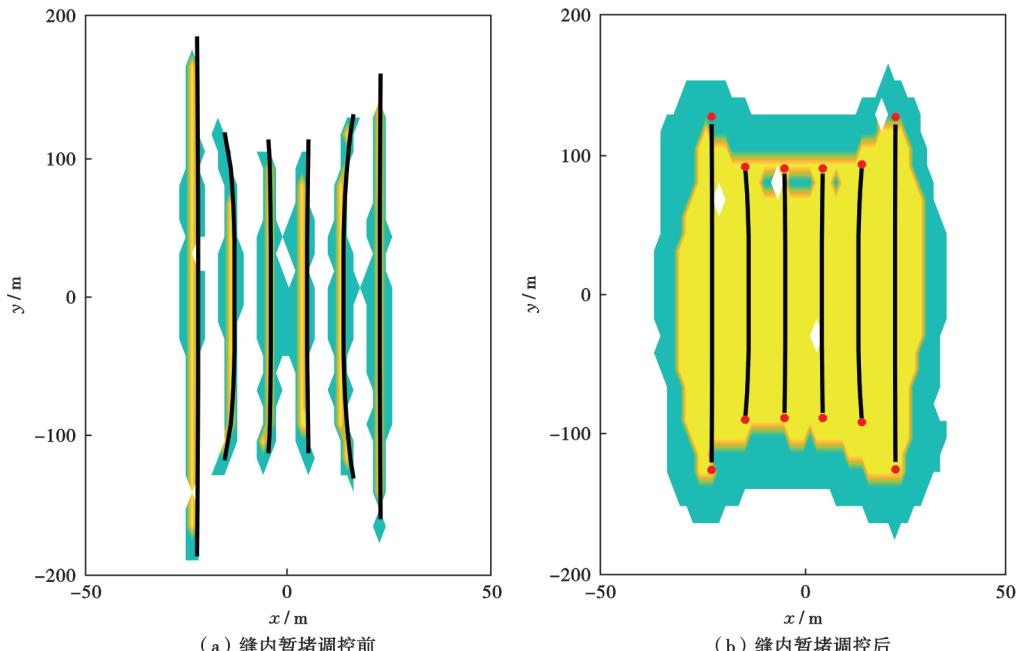
针对采用滑溜水 + 胶液混合注入模式缝网复杂性低、高浓度支撑剂输运铺置困难、摩阻大、井口施工压力高等问题,需要研发适应深层—超深层页岩气压裂



注:条带表示水力裂缝,颜色越接近红色,缝宽越大;颜色越接近蓝色,缝宽越小。

图 12 缝口暂堵调控簇裂缝均匀延伸模拟

Fig. 12 Uniform propagation simulation of cluster fractures controlled by temporary blocking at fracture inlet



注:黑色线条表示水力裂缝;黄色区域表示发生张性破坏的储层改造区域;蓝色区域表示发生剪切破坏的储层改造区域。

图 13 缝内暂堵调控缝网复杂度模拟

Fig. 13 Complexity simulation of fracture network controlled by temporary blocking in fractures

的高携砂、低摩阻、耐盐、耐温、抗剪一体化变黏滑溜水体系^[130-132],工程上还需满足实时泵注、连续混配、重复利用的复合功能,实现一套滑溜水压裂既能低黏造缝扩网、又能高黏携砂撑网的目标。随着页岩气开发规模不断增大,压裂液用量大和水资源匮乏的矛盾将更加凸显,需要未雨绸缪,开发无水或少水压裂液体系(如 CO₂ 压裂液)。

4.6 国产工具可靠性研究并形成系列化

井下分段等工具推动了页岩气压裂发展^[133],但深层—超深层压裂工具要求抗压抗温能力更高,深层页岩气压裂工具国产化并提高可靠性是加速页岩气开发的关键环节。如中国石油西南油气田公司研发的全

金属可溶桥塞具有体积小、全金属设计、无胶筒部件、超大内径、快速溶解特征,通井时间较常规可溶桥塞显著缩短,作业时效显著提高。国产工具规模化应用既可以降低成本,又可以迫使国外公司进一步降低价格。

4.7 地质—钻井—压裂—经济一体化

目前地质—工程一体化主要是地质—评价一体化、地质—钻井一体化、地质—压裂一体化^[134],虽然一直在提地质—工程一体化,但实践中更多的仍然是“各司其职、互不耦合”。地质—工程一体化的实质是寻求页岩气开发甜点,而地质甜点、钻井甜点、压裂甜点、经济甜点的交集才是真正的页岩气开发甜点(图 14)^[28]。其中,压裂甜点是在精细评价缝网可压性基础上,精准

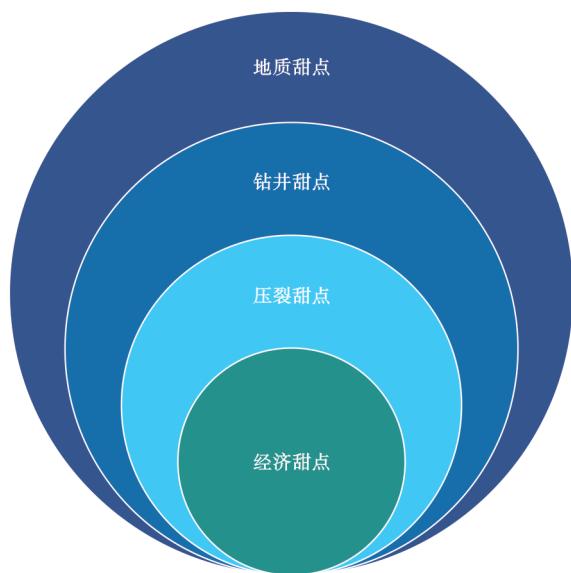
图 14 页岩气开发甜点^[28]

Fig. 14 Shale gas development sweet spot

模拟缝网体积,差异化设计关键参数,实现一区一案、一井一案,一段一策、一簇一策的精细化压裂设计。

4.8 焖井与排采制度优化技术

制定最佳焖井时间,制订合理的气井返排生产制度是深层—超深层页岩气井优化配产、提高单井 EUR 的关键环节。页岩水化促进内部裂缝扩展^[135],焖井过程中气藏温度回升联合水化效应,将提升缝网复杂度和页岩流动能力,需要加强页岩水化研究优化焖井时间^[136]。建立气水两相返排生产流动模型(图 15),结合井筒携液理论,研究压裂液返排和全生命周期生产特征,构建深层—超深层页岩气压后排采技术。

4.9 深层页岩气井长期稳产技术

相比美国典型页岩气藏,中国页岩气藏吸附气占比高。川南地区深层吸附气占比总体比中浅层低,但埋深越大,吸附气占比又呈增大趋势^[137]。深层—

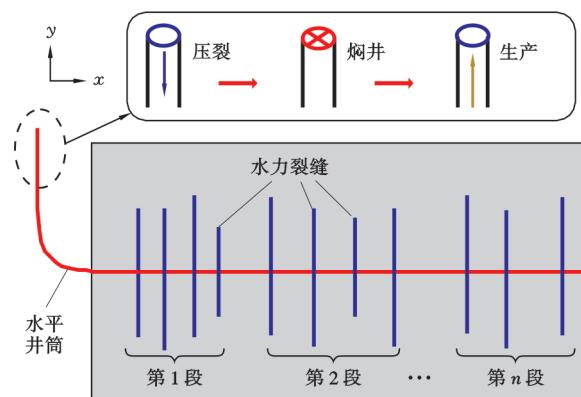


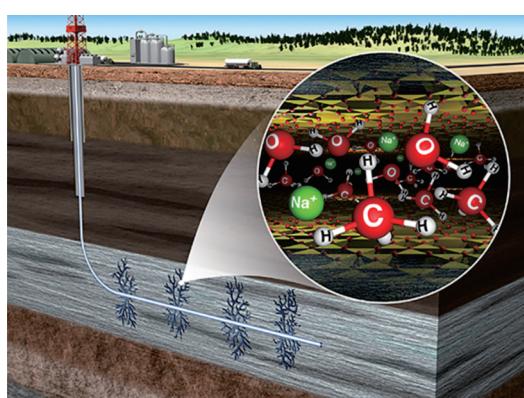
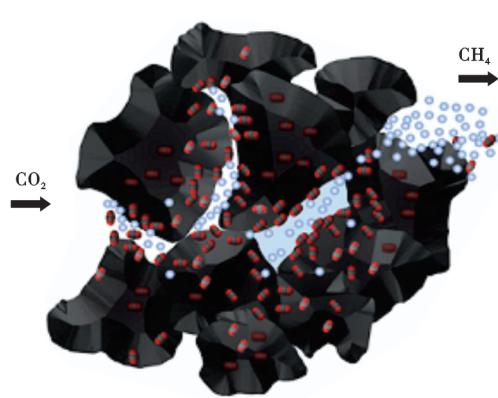
图 15 压裂—焖井—排采一体化物理模型

Fig. 15 Integrated physical model of fracturing, shut-in, drainage and production

超深层天然裂缝发育程度低、地应力大、缝网建造更加困难,压降在储层中的传播受到了明显抑制,深部吸附气难以受到压降波及形成高效解吸,仅靠自然解吸无法保证页岩气长期稳产^[138-139]。需要开展页岩气解吸机理和解吸技术研究,掌握不同生产阶段吸附气动用规律。如可以充分利用页岩对 CO₂ 的吸附能力远大于 CH₄ 的特性,开展纳米超临界 CO₂ 压裂—置换—增渗驱替协同提高页岩气采收率研究试验(图 16),实现 CO₂ 压裂—置换—驱气—埋存一体化^[140-141]。

4.10 套变及压窜防控技术

受区域断层、天然地震和高应力环境影响,需要研究深层—超深层页岩气地质稳定性及套变机理和套变防治技术,形成有效预防控制措施^[142-145]。压前套变井以研究长段和压裂缝调控为方向;压裂套变风险井以研究压裂诱发套变力学机理及优化设计压裂参数为方向^[146]。压窜控制以研究压窜机理、优化开发单元井距精细压裂设计降低压窜风险为主,优化经济、技术、管理一体化压窜综合应对方案。

(a) 页岩气 CO₂ 压裂示意(b) 页岩气 CO₂ 置换示意图 16 页岩气 CO₂ 压裂/置换示意^[140-141]Fig. 16 Schematic diagram of shale gas CO₂ fracturing/replacement

5 结束语

北美(美国)页岩气革命的巨大成功改变了世界能源格局。中国页岩气革命也取得阶段性胜利,已实现中浅层海相页岩气规模效益开发,深层—超深层页岩气已展现出巨大潜力。中浅层页岩气继续稳产上产和提高采收率是中国页岩气发展的“压舱石”,深层—超深层页岩气有效开发是中国页岩气发展的主战场,需要“深浅并重”,向深层—超深层进军,但机遇和挑战并存,尚需不断“砺剑”,加快建立中国深层—超深层页岩气压裂理论与技术体系。中国页岩气革命虽然面临诸多挑战,特别是深层—超深层页岩气开发难度更大,成本更高,但通过不断持续攻关和创新升级,国家延续相关税费扶持政策和加大补贴力度,中国页岩气产业一定会迎来再一次快速发展,获得页岩气开发新的突破,取得页岩气革命的更大胜利。

符号注释: σ_c —试样所承受的围压, MPa; σ_a —试样所承受的轴向应力, MPa; ϵ —应变; ϵ_a —试样轴向应变; ϵ_r —试样径向应变。

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